<u>**PATENT**</u>

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

Application No.:	10/812,406
Filing Date:	March 26, 2004
Applicant:	TAKASE et al.
Group Art Unit:	1742
Examiner:	MORILLO, Janelle Combs
Title:	WEAR-RESISTANT ALUMINUM ALLOY EXCELLENT IN CAULKING PROPERTY AND EXTRUDED PRODUCT...
Attorney Docket:	8498-000004/CO

Commissioner for Patents
P.O. Box 1450
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<u>SUPPLEMENTAL AFFIDAVIT OF KAZUHIRO NISHIKAWA TRAVERSING</u>
<u>REJECTION UNDER 37 CFR 1.132</u>

Sir:

I, Kazuhiro NISHIKAWA, state as follows:

1.   I graduated from Toyama University in 1983 with a bachelor's degree in Light Metal Engineering.

2.   In 1983, I started working for AISIN KEIKINZOKU CO., LTD. as an engineer in the Technical Development Department. My current position is Deputy General Manager of Production Control Department.

3.   I am an inventor of the subject matter claimed In the above-identified patent application.

4.   The claimed Invention Is directed to a wear-resistant aluminum alloy or extruded product that Is excellent In caulking properties.

5.   The composition of the alloy and extruded product of the claimed invention includes 0.1 to 0.39 wt% of Mg, 3.0 to 6.0 wt% of Si, 0.01 to 0.20 wt% of Cu, 0.01 to 0.5 wt% of Fe, 0.01 to 0.15 wt% of Mn, 0.01 to 0.5 wt% of Cr, less than 0.02 wt% of Zn, and the remainder being Al and unavoidable impurities.

6.   The wear-resistant aluminum alloy and extruded product having the composition of paragraph 5 are suitable for use in automotive break parts for which wear resistance to sliding parts and viscosity during plastic deformation such as caulking are required.

7.   To evaluate caulking properties of the alloy or extruded product, the calculation of a critical upsetting ratio may be used. The critical upsetting ratio occurs when microcracks develop during compression of the alloy or extruded product.

8.   The critical upsetting ratio of the alloy and extruded product of the claimed invention Is greater than or equal to 43%.

9.   The composition of the claimed invention also satisfies the numerical expression $0.79 \cdot (wt\% \text{ of } Mn) + 0.26 \cdot (wt\% \text{ of } Mg) \leq 0.22$, which significantly affects the critical upsetting ratio as shown in Figure 4 of the present application.

10. The coefficients 0.79 (Mn) and 0.26 (Mg) were calculated using a multiple regression analysis of the relationship between the critical upsetting ratio as an evaluation item of caulking properties and the alloy components.

11. The critical upsetting ratio is significantly affected by the Mg content and the Mn content in the claimed ranges of 0.1 to 0.39 wt% and 0.01 to 0.15 wt%, respectively.

12. Reference Figure 1 (attached at Exhibit A) shows the relationship between the expression 0.79·(wt% of Mn)+0.26·(wt% of Mg) using the coefficients calculated using the multiple regression analysis and the critical upsetting ratio (%).

13. As can be seen in Reference Figure 1, the horizontal axis indicates the value of 0.79·(wt% of Mn)+0.26·(wt% of Mn), and the vertical axis indicates the critical upsetting ratio (%).

14. The plot numbers shown in Reference Figure 1 indicate Nos. 1 to 10 shown in Figure 1 of the present application, and supplemental data Nos. 11 to 18 as comparative examples.

15. The supplemental data Nos. 11 to 18 were selected from the ranges disclosed in the cited reference JP 09-176769 ('769).

16. The alloy I of JP '769 (No. 9 in Table 2-1) contains Mg in an amount of 0.40 wt%, which is greater to a small extent than the upper limit (0.39 wt%) for Mg of the claimed invention, and contains Mn in an amount within the range of the claimed invention. Therefore, alloy I of JP '769 (No. 9 in Table 2-1) is the prior art closest to the present invention.

17.   Reference Figure 2, attached as Exhibit B shows the alloy compositions and the critical upsetting ratios of the supplemental data Nos. 11 to 18.

18.   As is clear form Reference Figure 1, alloy Nos. 1 to 6, 8 and 9 according to the claimed Invention and the supplement data Nos. 11 to 18 (comparative examples selected from JP '769) clearly belong to different groups.

19.   When the value indicated by the horizontal axis is x and the value indicated by the vertical axis is y, alloy Nos. 1 to 6, 8 and 9 according to the claimed Invention belong to a first group approximated by $y = -100.46x + 65.55$ ($R^2 = 0.84$, linearly approximated statistically), and the supplemental data Nos. 11 to 18 belong to a second group approximated by $y = -13.40x + 43.68$ ($R^2 = 0.50$, almost linearly approximated statistically).

20.   The minimum upsetting ratio of the alloys according to the claimed Invention shown in Figure 1 is 43.1%. In this case, the value of $0.79 \times Mn + 0.26 \times Mg$ is 0.22 (upper limit).

21.   In contrast, the supplemental data Nos. 11 to 18 which were selected from JP'769 have a value of 0.79(wt% of Mn) +0.26(wt% of Mg) of more than 0.22, as shown in Reference Figure 1.

22.   Supplemental data No. 16 was prepared to coincide with alloy I of JP '769 (No. 9 in Table 2-1), but differs from the alloy I of JF '769 as to the Si, Fe, and Ti content by 0.02 wt%. This is the difference between the amount of component added when adding each component to pure aluminum and casting

an aluminum alloy and the amount of component determined by analyzing the produced aluminum alloy.

23. The supplemental data Nos. 16-18 contain a Mg content that is just slightly outside of the claimed range of 0.39 wt%.

24. Supplemental data Nos. 16 to 18 was prepared as data representing JP '769. The Mg and Mn ranges of the experimental data Nos. 17 and 18 were almost the same as those of the experimental data No. 16. On the other hand, the Si content was increased in the order of No. 16. (Si: 4.04 wt%), No. 17 (Si: 4.52 wt%), and No. 18 (Si: 4.98 wt%).

25. Surprisingly, critical upsetting ratios of the experimental data Nos. 16 to 18 are smaller to a large extent than the value (43% or more) defined in the claimed invention, as shown in Reference Figure 1.

26. Quite unexpectedly, even though the comparative alloy Nos. 11 to 18 that were taken from the alloys disclosed JP '769, and in particular alloy Nos. 16-18 have a Mg content that is very close to the claimed range of 0.39 wt%, only the critical upsetting ratio of the claimed combination is greater than or equal to 43%.

Respectfully submitted,

Date: _July. 31. 2007_ By: _Kazuhiro Nishikawa_
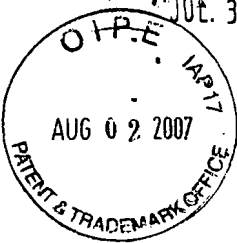Kazuhiro NISHIKAWA

Reference Figure 1

Critical Upsetting Ratio (%)

$y = -100.4G \times x + 65.55$
$R^2 = 0.84$

$y = -13.40 \times x + 43.68$
$R^2 = 0.50$

$0.79 \times Mn + 0.26 \times Mg$

No.5, 0.11, 53.9
No.2, 0.13, 51.6
No.1, 0.18, 49.2
No.9, 0.20, 49.8
No.6, 0.17, 49.0
No.3, 0.20, 48.8
No.4, 0.18, 47.2
No.8, 0.22, 43.1
No.11, 0.26, 40.8
No.14, 0.29, 40.3
No.10, 0.27, 40.2
No.13, 0.32, 38.6
No.12, 0.35, 38.4
No.17, 0.25, 40.6
No.16, 0.25, 40.1
No.18, 0.26, 39.3
No.15, 0.24, 38.9
No.7, 0.43, 44.5

more than or equal to 43%

less than or equal to 0.22
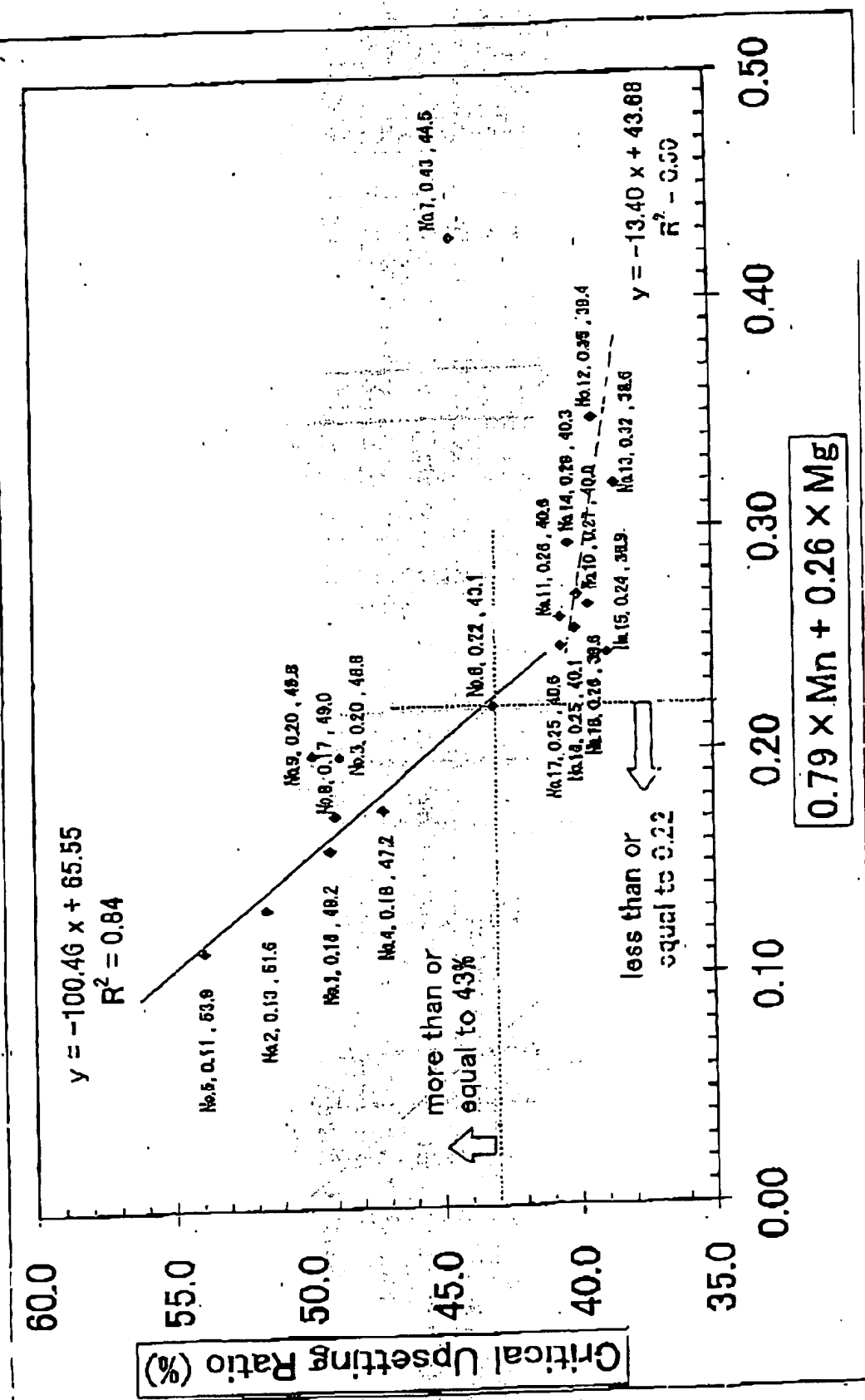
Reference Figure 2

	NO.	COMPONENTS (%)								CRETICAL UPSETTING RATIO(%)
		Si	Fe	Cu	Ti	Mn	Mg	Cr	Zn	
COMPARATIVE EXAMPLE	11	3.85	0.28	0.15	0.03	0.16	0.51	C.15	0.01	40.6
	12	4.96	0.29	0.16	0.04	0.24	0.61	C.14	0.00	39.4
	13	3.97	1.06	0.14	0.03	0.20	0.62	C.10	0.01	38.6
	14	4.17	0.29	0.96	0.03	0.18	C.58	C.1C	0.01	40.3
	15	4.59	0.30	0.15	0.03	0.11	0.60	C.1C	0.01	39.9
	16	4.04	0.30	0.15	0.03	0.19	0.40	C.15	0.01	40.1
	17	4.52	0.29	0.16	0.04	0.18	0.40	C.15	0.01	40.6
	18	4.98	0.28	0.15	0.03	0.20	0.41	C.10	0.01	39.6